	1	•		INDL	an S	PACE	E RES	FAR	сн С						Page
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	201	1			М	ECHA	NICAL	ENGI	NEER	LING -	11			S	ET -
1.	<u>Lis</u> A. B.	s <u>t I</u> Pelto Franc	ist I w n whe cis Tur an Tur	el (sin bine	•			<u>List</u> ] 1. M 2. Hi	<u>II</u> lediun igh di	swer n disch scharge n disch	e, low	head		ad	• •
	a) b)	<b>A</b> 4	<b>B</b> 3 3 1 2	С 2				<b>4.</b> Lo	w dis	charge	, high ∣	nead			
2.		versil $v_2/v_1$		abati	c proc b) (	ess matrix $\left[ \upsilon_2 / \upsilon_1 \right]$	ay be exp $\int_{\gamma}^{\gamma-1/\gamma}$	xpress	sed as c) (p	$\int_{p_1/p_2}^{T} \left( \frac{T_1}{T} \right)$	$\binom{1}{2}$ equ	al to	<b>d</b> ) (j	$p_1/p_2)$	γ−1
	A														
<b>3.</b> <b>4</b> .	var a) A Ac a) N	iation A para cordi /lass a	of pr bola ng to f	essur b) A first la ergy a	e vs. v hyper w of t re mut	olume bola therm ually o	c) A odynan converti	straigl nics	ht line <b>b)</b> 1	throu Heat an	ıgh ori 1d wor	gin k are	d) N mutu	one of ally co	`these
•	var: a) A Ac a) N c) H	iation A para cordi /lass a	of pr bola ng to f und end ows fr	essur b) A first la ergy a	e vs. v hyper w of t re mut	olume bola therm ually o	e is c) A odynan	straigl nics	ht line <b>b)</b> 1	throu	ıgh ori 1d wor	gin k are	d) N mutu	one of ally co	`these
•	var a) A Ac a) M c) H S Picl a) D	iation A para cordi Aass a Ieat fl substa k up t	of pr bola ng to f und end ows fr nce	essur b) A first la ergy a om ho orrec diame	e vs. v hyper nw of t re mut of subs t state ter	olume bola herm ually o tance	e is c) A odynan converti	straigl <b>nics</b> ible trifug	b) d) gal pu b) H	throw Heat an Carnot	ngh ori nd wor engin speed)	gin k are is m	d) N mutu	one of ally co	`these
4.	var: a) A Acc a) M c) H S Picl a) D c) H	iation A para cordi Mass a leat fl substa k up t Discha lead o	bola ng to f nd end ows fr nce he inc $rge \alpha$ $\iota$ (dian	essur b) A first la ergy a om ho orrec diame neter) <sup>5</sup>	e vs. v hyper nw of t re mut ot subs t state ter	olume bola hermo ually o tance ment	e is c) A odynan converti to cold	straigl nics ible trifug	ht line b) d) gal pu b) H d) D	throw Heat an Carnot mps ead α ( ischarg	ngh ori nd wor engin engin speed) e α sp	gin k are e is m 2 eed	d) N mutu ost e	one of ally co	`these
<b>4.</b> 5.	var: a) A Ac a) M c) H S Picl a) C c) H If tl a) L	iation A para cordi Mass a leat fl substa k up t Discha lead c he dis Decrea	bola ng to f nd end ows fr nce he inc $rge \alpha$ $\iota$ (dian charg	essure b) A first la ergy a om ho orrec diame neter) <sup>5</sup> e of a	e vs. v hyper w of t re mut of subs t state ter centr	olume bola hermo ually o tance ment	e is c) A odynan converti to cold for cen	straigl nics ible trifug	b) d) al pu b) H d) D ottled b) Fi	throw Heat an Carnot mps ead α ( ischarg	ngh ori engin speed) e α sp ts suct reases	gin k are e is m 2 eed ion li	d) N mutu ost e	one of hally co fficien	these onvert
<b>4.</b> 5.	var: a) A Acc a) M c) H S Picl a) E c) H If tl a) E c) R A c area	iation A para cordi Mass a leat fl substa k up t Discha lead o he dis Decrea temai ylind a A h	bola ng to f nd end ows fr nce he inc rge $\alpha$ $\alpha$ (dian charg uses ns unc rical b eight $I$	essur b) A first la ergy a om ho correc diame neter) <sup>-</sup> e of a hange body o H and	e vs. v hyper nw of t re mut of subs t state ter d f cros the de	olume bola hermo tance ment ifugal s-secti ensity	e is c) A odynan converti to cold for cen pump	straigl nics ible trifug	b) d) al pu b) H d) D ottled b) Fi	throw Heat an Carnot mps ead α ( ischarg then i rst incl	agh ori and wori engine speed) $e \alpha$ sp ts such reases	gin k are e is m 2 eed ion li	d) N mutu ost e	one of hally co fficien	these onvert
<b>4.</b> 5.	var: a) A Acc a) M c) H S Picl a) E c) H If tl a) E c) R A cy are: imm den	iation A para cordi Mass a leat fl substa k up t Discha lead o he dis Decrea Lemai ylind a A h nerse sity A	bola ng to f nd end ows fr nce he inc rge $\alpha$ $\alpha$ (dian charg uses ns unc rical b eight $I$ d to a	essur b) A first la ergy a om ho correc diame neter) <sup>2</sup> e of a hange ody o 7 and depth tied t	e vs. v hyper nw of t re mut of subs t state ter d f cross the de th in a o the l	olume bola hermo tance ment ifugal s-secti ensity a liqui bottor	e is c) A odynam converting to cold for cen pump ional $\rho_s$ is d of n with :	straig nics ible trifug	b) d) al pu b) H d) D ottled b) Fi	throw Heat au Carnot mps ead α ( ischarg then i rst incu crease:	agh ori and wori engine speed) $e \alpha$ sp ts such reases	gin k are e is m 2 eed ion li	d) N mutu ost e ift nen de	one of hally co fficien	these onvert

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2	011	MECI	HANICA	L ENG	INEERING - II		SET - A
8.	carrying wate manometer sh	r. If the manon	netric li fference	quid is of 20	ential between tw s mercury (specif cm, then the pres	ic gravity 13	.6) and the
	<b>a)</b> 1.26 m	<b>b)</b> 2.72	m		<b>c)</b> 1.36 m	<b>d</b> ) 2.	52 m
9.	, <b>.</b>	ice at Reynolds 0.001 and 0.002.			500 in two differe factor	nt pipes with	n relative
•	<ul><li>b) Will be h</li><li>c) Will be t</li></ul>	higher for the pip he same in both	be having the pipe	g relati s	roughness of 0.00 ve roughness of 0 the basis of data	.002	
10.	A liquid com 0.039 m <sup>3</sup> at 15	pressed in cylin 50 kg/cm <sup>2</sup> . The	der has bulk m	a volu odulu:	me of 0.04 m <sup>3</sup> at s of elasticity of li	50 kg/cm <sup>2</sup> an iquid is	nd a volume o
	<b>a)</b> 400 kg/cm <sup>2</sup>	<b>b)</b> 40 2		/cm <sup>2</sup>	<b>c)</b> 40 x 10 <sup>5</sup> kg/c	$cm^2$ <b>d</b> ) 40	$000 \text{ kg/cm}^2$
11.	A fluid jet is	discharging fro 0 mm. If the c	k 10 <sup>6</sup> kg/ <b>m a 100</b>	mm n	c) 40 x 10 <sup>5</sup> kg/c nozzle and the ver elocity is 0.95, the	na contracta	formed has a
11.	A fluid jet is diameter of 9	discharging fro 0 mm. If the c	k 10 <sup>6</sup> kg/ m a 100 oefficier	mm n	ozzle and the ver	na contracta	formed has a cient of
11.	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develo	discharging fro 0 mm. If the c the nozzle is b) 0.81	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl	mm n nt of v ow thr	ozzle and the ver elocity is 0.95, the	na contracta en the coeffic d) 0.	formed has a cient of 855
	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develo	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl	mm n nt of v ow thr	c) 0.9025	na contracta en the coeffic d) 0.	formed has a cient of 855 ratio of
	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develo maximum ve a) 3.0 If the surface	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl e veloci er-air in	mm n nt of v ow thr ty as	ozzle and the ver elocity is 0.95, the c) 0.9025 ough a circular t	na contracta en the coeffic d) 0. ube has the d) 1.	formed has a cient of 855 ratio of 5
12.	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develo maximum ve a) 3.0 If the surface	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0 tension of wate 1 mm diameter	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl e veloci er-air in will be	mm n nt of v ow thr ty as	c) 0.9025 c) 2.5	na contracta en the coeffic d) 0. ube has the d) 1. e gauge pres	formed has a cient of 855 ratio of 5
12.	A fluid jet is of diameter of 9 discharge for a) 0.7695 A fully develop maximum ve a) 3.0 If the surface rain drop of a) 0.146 N/m <sup>2</sup>	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0 tension of wate 1 mm diameter b) 73 1	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl e veloci er-air in will be	mm n nt of v ow thr ty as	c) 0.9025 c) 2.5 c) 2.7 c) 2.7 c) 2.7 c) 2.5	na contracta en the coeffic d) 0. ube has the d) 1. e gauge pres d) 29	formed has a cient of 855 ratio of 5 ssure inside a 92 N/m <sup>2</sup>
12.	A fluid jet is of diameter of 9 discharge for a) 0.7695 A fully develop maximum ve a) 3.0 If the surface rain drop of a) 0.146 N/m <sup>2</sup>	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0 tension of wate 1 mm diameter b) 73 1	k 10 <sup>6</sup> kg/ m a 100 oefficien l scous fl e veloci er-air in will be N/m <sup>2</sup> y (x <sup>2</sup> – y	mm n nt of v ow thr ty as	c) 0.9025 rough a circular t c) 2.5 e is 0.073 N/m, th c) 146 N/m <sup>2</sup>	na contracta en the coeffic d) 0. ube has the d) 1. e gauge pres d) 29 ion of the flo	formed has a cient of 855 ratio of 5 ssure inside a 92 N/m <sup>2</sup>
12.	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develor maximum ve a) 3.0 If the surface rain drop of 2 a) 0.146 N/m <sup>2</sup> A stream fun a) $2xy + f(x)$ The temperat	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0 tension of wate 1 mm diameter b) 73 f ction is given by b) 2 (x ture profile bety	x $10^6$ kg/ m a 100 oefficien l scous fl e veloci er-air in will be N/m <sup>2</sup> y (x <sup>2</sup> - y y (x <sup>2</sup> - y <sup>2</sup> ) ween tw	mm n nt of v ow thr ty as terfac v <sup>2</sup> ). Th	c) 0.9025 rough a circular t c) 2.5 e is 0.073 N/m, th c) 146 N/m <sup>2</sup> he potential function c) -2xy + constants	na contracta en the coeffic d) 0. ube has the d) 1. d) 1. d) 29 ion of the flo ant d) 29	formed has a cient of 855 ratio of 5 ssure inside a 92 N/m <sup>2</sup> w will be
12. 13.	A fluid jet is a diameter of 9 discharge for a) 0.7695 A fully develor maximum ve a) 3.0 If the surface rain drop of 1 a) 0.146 N/m <sup>2</sup> A stream fun a) $2xy + f(x)$ The temperative together is sh	discharging fro 0 mm. If the c the nozzle is b) 0.81 oped laminar vi locity to averag b) 2.0 tension of water b) 73 f ction is given by b) 2 (x ture profile betw own in Fig. Fro	x $10^6$ kg/ m a 100 oefficien l scous fl e veloci er-air in will be N/m <sup>2</sup> y (x <sup>2</sup> - y y (x <sup>2</sup> - y <sup>2</sup> ) ween tw	mm n nt of v ow thr ty as aterfac <sup>2</sup> ). Th o meta igure i	<ul> <li>c) 0.9025</li> <li>c) 0.9025</li> <li>c) 2.5</li> <li>e is 0.073 N/m, the</li> <li>c) 146 N/m<sup>2</sup></li> <li>de potential function</li> <li>c) -2xy + constant</li> </ul>	a contracta en the coeffic d) 0. ube has the d) 1. e gauge pres d) 29 ion of the flo ant d) 22	formed has a cient of 855 ratio of 5 ssure inside a $92 \text{ N/m}^2$ w will be xy + f(y)

इस्	7	INDIAN	SPACE RESEA	RCH ORG	ANISATION	Page: 3 OF 1
2	011		MECHANICAL EN	GINEERING	- 11	S OF 1
16.	According equal to	to Fourier's	law, amount of h	eat flow (Q)	through the body i	n unit time i
	<b>a)</b> $KA\frac{dT}{dx}$	b	) $KA \frac{dT^2}{dx^2}$	c) $K \frac{dx}{dT}$	<b>d)</b> <i>K</i>	$A\frac{dx}{dT}$
17.	Pitch diam	eter is equal	to the product of			•
	•	pitch and nun e and number		· -	depth and number o nd number of teeth	fteeth
18.			e supporting a lift ds. What is the a		vards is twice the to f the lift?	ension when
	<b>a)</b> g/4	<b>b)</b> g/	′3	<b>c)</b> g/2	<b>d)</b> G	
19.	Whirling s	peed of a sha	ft coincides with	the natural f	frequency of its	•
	<ul><li>a) Transver</li><li>c) Torsiona</li></ul>			, .	inal vibration bending torsional vi	bration
20.	time in seco maximum	onds. The tin displacement	ne taken by the pa t is		$x = 3\cos(0.25\pi t)$ , we from position of d) 3.0	equilibriun (
	<b>a</b> ) 2.0 sec	U) 1.	0 sec	<b>c)</b> 0.5 sec	u) 5.0	SEC
21.		cts are weigh 5 must have i		ooth of them	lose the same weig	ht, then the
	a)Specific g	gravities	<b>b)</b> Weights in a	ir c) Dens	ities d) Vol	umes
22.	The vapou	r pressure at		e 0.025 bar a	tant pressure of 1 t nd 0.0087 bar. Th	
	<b>a)</b> 66%	<b>b)</b> 85%	/ 0	<b>c)</b> 51%	<b>d</b> ) 17%	•
23.	ratio of 2:1	. Both are he	eated to same tem	perature and	sh have their diam d allowed to cool by e will be in the ratio	y radiation.
	<b>a)</b> 1:2	<b>b)</b> 2:1		<b>c)</b> 1:1	<b>d</b> ) 4:1	······································
24.		÷ .	at 0 <sup>0</sup> C are compl heat of fusion is	-	Find the entropy	change, in
	-) ()	<b>b</b> ) 45		<b>c)</b> 105	<b>d</b> ) 85	
	<b>a</b> ) 0	0,40				

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2	2011	MECHANICA	L ENGINEERING - II		SET - A
25.		ft of 100mm diameter tra 5 ×10 <sup>5</sup> kg/cm <sup>2</sup> .Then the n	-	-	
	<b>a</b> ) 5 <sup>0</sup>	<b>b</b> ) 2.5 <sup>0</sup>	<b>c)</b> 3.2 <sup>0</sup>	<b>d)</b> 2 <sup>0</sup>	
26.	A perfect g temperatur	gas at 27 <sup>0</sup> C is heated at co re is	onstant pressure till its	volume is double	. The final
	<b>a)</b> 54 <sup>0</sup> C	<b>b</b> ) 108 <sup>0</sup> C	<b>c)</b> 327 <sup>0</sup> C	<b>d)</b> 600 <sup>0</sup> C	
27.	. –	tion temperature of an is e is 200 K at a section, th			
	<b>a)</b> 1.0	<b>b</b> ) 1.5	<b>c)</b> 3.0	<b>d)</b> 2.0	· ·
28.	Air at 20 <sup>0</sup> C	blows over a plate of 50	cm X 75 cm maintaine	ed at 250 <sup>0</sup> C. If th	e
	convection	heat transfer coefficient	is $25W/m^{2^0}C$ , the heat	transfer rate is	
	<b>a)</b> 2.156 kW	<b>b)</b> 2156 kW	<b>c)</b> 215.6 kW	<b>d)</b> 21.56 k	W, ·
29.		stic boat loaded with piec	es of steel rods is floati	ng in a bath tub.	If the
	tub will		ving the boat to float en	npty, the water le	vel in the
	tub will	nped into the water allow ) Remains same c) Fall		npty, the water le	vel in the
30.	tub will a) Rise b) When a jet top of its tra passenger is the radius of	Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we s one half of her actual w of curvature R of the fligh	d) Cannot be estin at the very eight of a reight. Find	npty, the water le	vel in the
30.	tub will a) Rise b) When a jet top of its tra passenger is the radius of	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we s one half of her actual w	d) Cannot be estin at the very eight of a reight. Find	npty, the water le	vel in the
<b>30.</b> <b>31.</b>	<ul> <li>tub will</li> <li>a) Rise b)</li> <li>When a jet top of its trapassenger is the radius of this point.</li> <li>a) 22 km</li> <li>Two cars an 10 km separation of the separation of the</li></ul>	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we s one half of her actual w of curvature R of the fligh Use g= 10 m/s <sup>2</sup>	d) Cannot be estin a at the very eight of a reight. Find ht path at c) 30 km rection with a speed of ing from the opposite d	npty, the water le nated from the info R d) 16 km 45 km/hr and a d	vel in the ormation istance of
	<ul> <li>tub will</li> <li>a) Rise b)</li> <li>When a jet top of its trapassenger is the radius of this point.</li> <li>a) 22 km</li> <li>Two cars an 10 km separation of the separation of the</li></ul>	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we s one half of her actual w of curvature R of the fligh Use g= 10 m/s <sup>2</sup> b) 18 km re moving in the same dia rates them. If a car com	d) Cannot be estin a at the very eight of a reight. Find ht path at c) 30 km rection with a speed of ing from the opposite d	npty, the water le nated from the info R d) 16 km 45 km/hr and a d	vel in the ormation istance of ese two
	<ul> <li>tub will</li> <li>a) Rise b)</li> <li>When a jet top of its trapassenger is the radius of this point.</li> <li>a) 22 km</li> <li>Two cars an 10 km separation of the radius of</li></ul>	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we s one half of her actual w of curvature R of the fligh Use g= 10 m/s <sup>2</sup> b) 18 km re moving in the same dim rates them. If a car commuter nterval of 6 minutes, its s	<ul> <li>d) Cannot be estimated at the very eight of a reight. Find hat c) 30 km</li> <li>c) 30 km</li> <li>rection with a speed of the opposite depeed would be c) 65 km/hr</li> </ul>	npty, the water le nated from the info R d) 16 km 45 km/hr and a d irection meets the d) 75 km/hr another rim type	vel in the ormation istance of ese two
31.	<ul> <li>tub will</li> <li>a) Rise b)</li> <li>When a jet top of its trapassenger is the radius of this point.</li> <li>a) 22 km</li> <li>Two cars an 10 km separation of the rotation of the</li></ul>	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we sone half of her actual w of curvature R of the fligh Use g= 10 m/s <sup>2</sup> b) 18 km re moving in the same dif rates them. If a car comin terval of 6 minutes, its s b) 55 km/hr ing mass of a rim type fly a radius is half the mean	<ul> <li>d) Cannot be estimated at the very eight of a reight. Find hat c) 30 km</li> <li>c) 30 km</li> <li>rection with a speed of the opposite depeed would be c) 65 km/hr</li> </ul>	npty, the water le nated from the info R d) 16 km 45 km/hr and a d irection meets the d) 75 km/hr another rim type hen energy stored	vel in the ormation istance of ese two
31.	<ul> <li>tub will</li> <li>a) Rise b)</li> <li>When a jet top of its trapassenger is the radius of this point.</li> <li>a) 22 km</li> <li>Two cars an 10 km separation of the rotation of the</li></ul>	) Remains same c) Fall plane flying at 300 m/s is ajectory, the apparent we sone half of her actual we of curvature R of the fligh Use g= 10 m/s <sup>2</sup> b) 18 km re moving in the same din rates them. If a car commin terval of 6 minutes, its s b) 55 km/hr ing mass of a rim type fly a radius is half the mean same speed will be	d) Cannot be estin at the very eight of a reight. Find ht path at c) 30 km rection with a speed of ing from the opposite d peed would be c) 65 km/hr wheel is distributed on radius of the former, th	npty, the water le nated from the info R d) 16 km 45 km/hr and a d irection meets the d) 75 km/hr another rim type hen energy stored first one	vel in the ormation istance of ese two

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×.		BATCOLLANICA	L ENGINEERING - II	5 OF 13 SET - A
<b>4</b>		MECHANICA		
.33.	Tungsten in High	Speed Steel provi	des	
	a) Hot hardness	b) Toughness	c) Wear resistance d) Sl	harp cutting edge
34.		llowing regions of ucture of crystallin	the electromagnetic spectrum e solids?	n would be used
	a) Microwave	b) Infrared	•	d) Visible
35.	Fluidity in casting	g (CI) operation is	greatly influenced by	
		ature of molten met		
36.	Robert Hooke dis	scovered experime	ntally that within elastic limit	
	a) Stress = strain		<b>b</b> ) Stress/strain = a cons	tant
	c) Stress x strain =	• 1	d) None of these	
28	TT 1		and all has also fix of low other 7 7	and I and the
37.	•	ameters are $d_1$ , $d_2$ a	nected by shafts of lengths $l_1, l_2$ and $d_3$ . this system is reduced to	•
37.	corresponding dia equivalent length a) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^4 + l_2^4$	ameters are $d_1$ , $d_2$ a of the shafts is		a torsionally
37.	corresponding dia equivalent length a) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^4 + l_2^4$	ameters are $d_1$ , $d_2$ a of the shafts is	nd $d_3$ . this system is reduced to	a torsionally
37.	corresponding di equivalent length	ameters are $d_1$ , $d_2$ a of the shafts is	nd $d_3$ . this system is reduced to b) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^3 + l_3 \left(\frac{d_1}{d_3}\right)^3$	a torsionally
37.	corresponding dia equivalent length a) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^4 + l_2$ c) $\frac{l_1 + l_2 + l_3}{3}$	ameters are $d_1$ , $d_2$ a of the shafts is	nd $d_3$ . this system is reduced to b) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^3 + l_3 \left(\frac{d_1}{d_3}\right)^3$ d) $l_1 + l_2 + l_3$	a torsionally
	corresponding dia equivalent length a) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^4 + l_2$ c) $\frac{l_1 + l_2 + l_3}{3}$	ameters are $d_1$ , $d_2$ a of the shafts is $d_3 \left(\frac{d_1}{d_3}\right)^4$ dening is applicable	nd $d_3$ . this system is reduced to b) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^3 + l_3 \left(\frac{d_1}{d_3}\right)^3$ d) $l_1 + l_2 + l_3$	a torsionally
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38.	corresponding dia equivalent length a) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^4 + l_2$ c) $\frac{l_1 + l_2 + l_3}{3}$ Precipitation har a) Pure aluminuin c) Non-metal Match the lists I a A. Car dash boar B. Aircraft wind C. Conduit pipes D. Bearings and A B	ameters are $d_I$ , $d_2$ a of the shafts is $f_3\left(\frac{d_1}{d_3}\right)^4$ dening is applicable and II using code g rd ows gears C D 3 4 1 2	nd $d_3$ . this system is reduced to b) $l_1 + l_2 \left(\frac{d_1}{d_2}\right)^3 + l_3 \left(\frac{d_1}{d_3}\right)^3$ d) $l_1 + l_2 + l_3$ le for b) Low carbon steel d) Aluminium – Copper given below 1. Polyvinylchloride (P 2. TEFLON 3. Polyacrylonitrile	a torsionally ) <sup>3</sup> alloy <b>YVC</b> )



through an edge

**a)** 
$$\frac{mb^2}{2}$$
 **b)**  $\frac{mb^2}{6}$  **c)**  $\frac{3mb^2}{2}$  **d)**  $\frac{2mb^2}{3}$ 

41. A thin cylinder contains fluid at a pressure of 30 kg/cm<sup>2</sup>. The inside diameter of the shell is 60 cm and the tensile stress in the material is to be limited to 900 kg/cm<sup>2</sup>. The shell must have minimum wall thickness of

**a**) 1mm **b**) 2.7mm **c**) 10mm **d**) 9mm

- 42. When a shaft is subjected to combined twisting moment (T) and bending moment (M), the equivalent twisting moment is equal to
  - a)  $\frac{1}{2} \Big[ M + \sqrt{M^2 + T^2} \Big]$ b)  $\sqrt{M^2 + 4T^2}$ c)  $\sqrt{4M^2 + T^2}$ d)  $\sqrt{M^2 + T^2}$

43. Two blocks with masses M and m are in contact with each other and are resting on a horizontal frictionless floor. When horizontal force F is applied to the heavier, the blocks accelerate to the right. The force between the two blocks are



d) (M+m)F/ma)  $\frac{mF}{(M+m)}$  b)  $\frac{MF}{m}$  c)  $\frac{mF}{M}$ 

44. A machine mounted on a single coil spring has a period of free vibration of T. If the spring is cut into four equal parts and placed in parallel and the machine is mounted on them, then the period of free vibration of the new system will be

**a**) 16 T **b**) T/4 **c**) 4 T **d**) T/16

## 45. Dislocations in materials are

a) Point defect	b) Surface defect	c) Planer defect	d) Line defect
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- 46. Which of the following thermocouple is capable of measuring highest temperature?
  - a) Chromel alumel
- b) Platinum rhodiumd) Iron constantan

c) Iridium – rhodium

Mechanical - II

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2	011	· · · · · ·	MECHANIC	AL ENGI	NEERING - II		SET - A	
59.	link plane	-	e of freedom on with five rev n with five rev e figure is		5	4	$\frac{3}{2}$	 
	<b>a)</b> 3		<b>b)</b> 4	•	<b>c)</b> 1	<b>)</b> d) 2		
<b>C</b> 0	<b>T</b>		- in a contary is	Ar it is a	ccontial that	holix angle is		
60.		-	g in a screw ja	ick, it is e	b) None of t			
,		than friction o friction ang				han friction ang	çle	• •
61.	A cutting	tool having	tool signatur	e as 10, 9,	, 6, 6, 8, 8, 2 v	will have side 1	ake angle	
·	<b>a)</b> 10°	н Настания Настания	<b>b)</b> 9°		<b>c</b> ) 8°	<b>d</b> ) 2	0	•••••••
62.	In radiog	raphic test,	type of defect	not detec	ctable by X-F	Ray is	,	•
	a) Delami	nation in clao en inclusion i	dded sheet	•	<b>b</b> ) Porosity i		relding	2 
63.	In CAM,	" Part prog	ramming" rel	fers to				
	a) Genera	tion of cutter 1 data	r b) On-line Inspectio		c) Machine Selectior		ol Selection	· ·
	location	and the second second						A
64.	A 50mm minutes. Assuming	The speed	ne relationshi	ed to 232	rpm and t	the tool failed	e occurred in 1 1 in 60 minutes life, the value o	5.
64.	A 50mm minutes. Assuming	The speed g straight lin	l was change ne relationshi	ed to 232 ip betwee	rpm and t	the tool failed	l in 60 minutes life, the value o	5.
<b>64.</b> <b>65</b> .	A 50mm minutes. Assuming Tayloriar a) 0.21 Which of direction	The speed g straight lin i Exponent i the followin	I was change ne relationshi is b) 0,13	ed to 232 ip betwee	2 rpm and f en cutting sp c) 0.11 oted for powe	the tool failed beed and tool d) ( er transmission	l in 60 minutes life, the value o ).23	5.
	A 50mm minutes. Assuming Taylorian a) 0.21 Which of	The speed g straight lin h Exponent i the followin threads	I was change ne relationshi is b) 0,13	ed to 232 ip betwee	2 rpm and t en cutting sp c) 0.11	the tool failed beed and tool d) ( er transmission chreads	l in 60 minutes life, the value o ).23	5.
	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acmet c) Square	The speed g straight lin i Exponent i the followin threads threads	I was change ne relationshi is b) 0,13	ed to 232 ip betwee ad is adag	<ul> <li>2 rpm and f</li> <li>2 rpm and f</li> <li>2 rpm and f</li> <li>3 rpm and f</li> <li>4 rpm and f</li> <li>4 rpm and f</li> <li>5 rpm and f</li> <li>6 rpm and f</li> <li>7 rpm and f</li> <li>8 rpm and f</li> <li>8 rpm and f</li> <li>9 rpm and f</li> <li></li></ul>	the tool failed beed and tool d) ( er transmission threads threads	l in 60 minutes life, the value o ).23	5.
65.	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acmet c) Square	The speed g straight lin i Exponent i the followin threads threads ue and RMS	I was change ne relationshi is b) 0,13 ng screw threa	ed to 232 ip betwee ad is adag	<ul> <li>2 rpm and to</li> <li>2 rpm and to</li> <li>2 rpm and to</li> <li>3 rpm and to</li> <li>4 rpm and to</li> <li>4 rpm and to</li> <li>4 rpm and to</li> <li>5 rpm and to</li> <li>5 rpm and to</li> <li>6 rpm and to</li> <li>7 rpm and to&lt;</li></ul>	the tool failed and tool d) ( er transmission threads threads of s of tool edge	l in 60 minutes life, the value o ).23	5.
65.	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acme t c) Square CLA valu a) Metal h	The speed g straight lin i Exponent i the followin threads threads ue and RMS	I was change ne relationshi is b) 0,13 ng screw threa values are us	ed to 232 ip betwee ad is adag	<ul> <li>c) 0.11</li> <li>b) Buttress t</li> <li>d) Multiple</li> </ul>	the tool failed and tool d) ( er transmission threads threads of s of tool edge	l in 60 minutes life, the value o ).23	5.
65.	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acmet c) Square CLA valu a) Metal H c) Surface	The speed g straight lin i Exponent i the followin threads threads ie and RMS hardness	I was change ne relationshi is b) 0,13 ng screw threa	ed to 232 ip betwee ad is adag	<ul> <li>2 rpm and to</li> <li>2 rpm and to</li> <li>2 rpm and to</li> <li>3 rpm and to</li> <li>4 rpm and to</li> <li>4 rpm and to</li> <li>4 rpm and to</li> <li>5 rpm and to</li> <li>5 rpm and to</li> <li>6 rpm and to</li> <li>7 rpm and to&lt;</li></ul>	the tool failed and tool d) ( er transmission threads threads of s of tool edge	l in 60 minutes life, the value o ).23	5.
65. 66.	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acmet c) Square CLA valu a) Metal H c) Surface	The speed g straight lin i Exponent i the followin threads threads and RMS hardness e dimensions r is specified	I was change ne relationshi is b) 0,13 ng screw threa	ed to 232 ip betwee ad is adag	<ul> <li>2 rpm and f</li> <li>2 rpm and f</li> <li>2 en cutting sp</li> <li>c) 0.11</li> <li>b) Buttress t</li> <li>d) Multiple</li> <li>casurement o</li> <li>b) Sharpness</li> <li>d) Surface re</li> </ul>	the tool failed and tool d) ( er transmission threads threads of s of tool edge	l in 60 minutes life, the value o ).23	5.
65. 66.	A 50mm minutes. Assuming Taylorian a) 0.21 Which of direction a) Acme t c) Square CLA valu a) Metal h c) Surface A sine ba a) Its tota	The speed g straight lin i Exponent i the followin threads threads ie and RMS hardness dimensions r is specified l length	I was change ne relationshi is b) 0,13 ng screw threa	ed to 232 ip betwee ad is adag	<ul> <li>2 rpm and f</li> <li>2 rpm and f</li> <li>2 en cutting sp</li> <li>c) 0.11</li> <li>b) Buttress t</li> <li>d) Multiple</li> <li>casurement of</li> <li>b) Sharpness</li> <li>d) Surface ro</li> <li>b) The size</li> </ul>	the tool failed and tool d) ( er transmission threads threads of s of tool edge oughness e of the rollers	l in 60 minutes life, the value o ).23	5.

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Page: INDIAN SPACE RESEARCH ORGANISATION इसरो डिल्व 10 of 11 2011 **MECHANICAL ENGINEERING - II** SET - A A shaft and hole pair is designated as 50H7d8. This assembly constitutes **68**. a) Interference fit b) Transition fit d) None of the above c) Clearance fit A milling machine has the following two index plates supplied along with the indexing 69. head: Plate I: 15, 16,17,18,19, 20, hole circles Plate 2: 21,23,27,29,31,33, hole circles It is proposed to mill a spur gear of 28 teeth using simple indexing method. Which one of the following combinations of index plate and number of revolutions is correct? Plate I: 1 revolution and 9 holes in 18 hole circles a) Plate 2: 1 revolution and 9 holes in 21 hole circles b) Plate 2: 1 revolution and 9 holes in 33 hole circles c) Plate 1: 1 revolution and 9 holes in 15 hole circles d) The initial blank diameter required to form a cylindrical cup of outside diameter 'd' 70. and total height 'h' having a corner radius 'r' is obtained using the formula a) Do=  $\sqrt{d^2 + 4 dh} - 0.5 r$ **b)** Do = d + 2h + 2rd)  $D_0 = \sqrt{d^2 + 4dh - 0.5r}$ c)  $Do = d^2 + 2h^2 + 2r$ 71. The equation of the tangent to the curve y(x-2)(x-3)-x+7=0, at the point where it cuts the x-axis is b) x + 20y = 7a) -x + 20v = 7d) -x - 20v = 7(c) x - 20 v = 772. If the imaginary part of  $\frac{2z+1}{iz+1}$  is -2, then the locus of the point z in the complex plane is **a)** x + 2y - 2 = 0**b)** 2x + y - 2 = 0**d)** x + 2y + 2 = 0c) x - 2y - 2 = 0General solution of the differential equation  $(D^2 - 2D + 1)y = e^x$  is 73. **b)**  $e^{x}(A+Bx)-\frac{x^{2}}{2}e^{x}$ **a)**  $Ae^{x} + Be^{-x} + \frac{x^{2}}{2}e^{x}$ **d**)  $e^{x}(A+Bx) + \frac{x^{2}}{2}e^{x}$ c)  $Ae^{x} + Be^{-x} - \frac{x^{2}}{2}e^{x}$ SET-A Mechanical - II

